

# IMDD vs Coherent

## Will Datacenter be the New Battleground?

Summer Topicals 2020 Virtual Conference

Tutorial TuA2.2 10:45AM – 11:30AM MDT

14 July 2020

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# Outline

- **NRZ vs HOM**
- Serial vs WDM
- Coherent in Telecom
- Coherent in Datacom
- IMDD vs Coherent SNR
- Intra Datacenter Optics
- Appendices

# Shannon-Hartley Theorem

$$C = B \log_2 (1 + S/N)$$

$C \triangleq$  Channel capacity

$B \triangleq$  Bandwidth

$S \triangleq$  Signal Power

$N \triangleq$  Noise Power

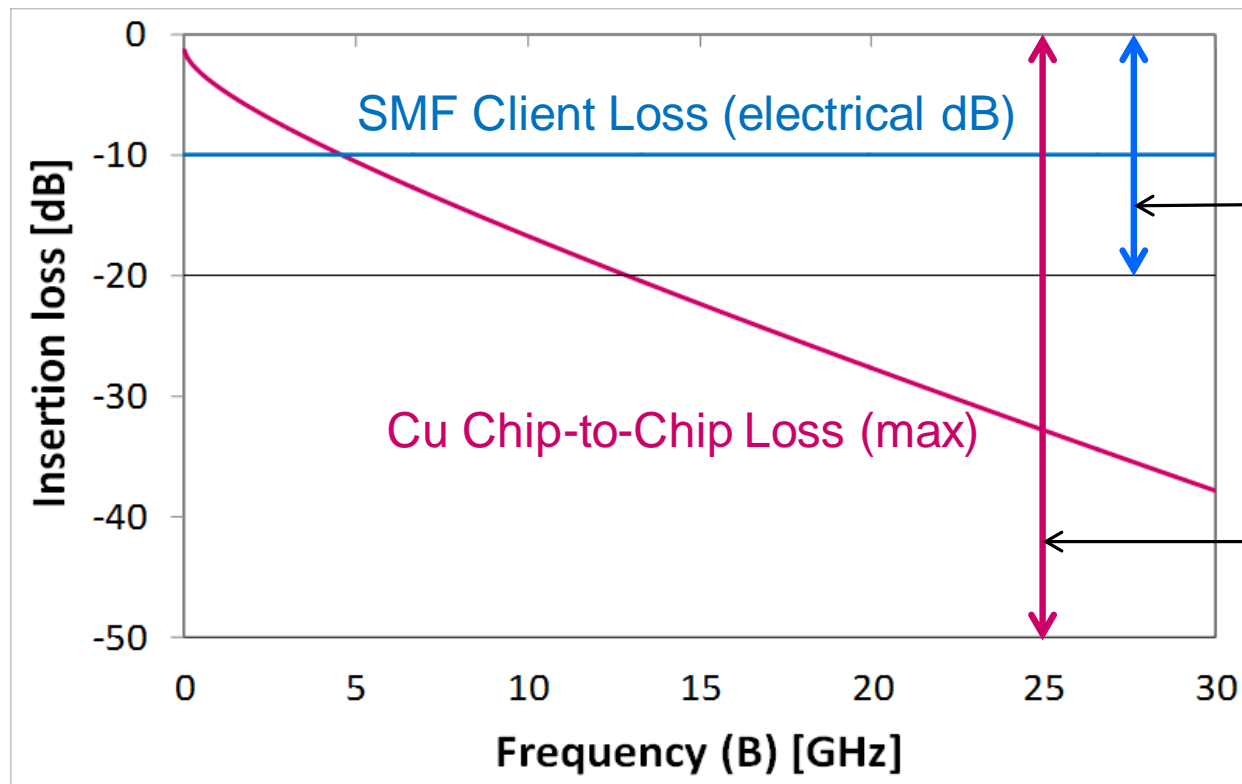
Guidance to increase C:

If B limited, use S/N to increase modulation order

If S/N limited, use B to increase Baud rate

C. Cole, "SMF PMD Modulation Observations", 400 Gb/s Ethernet Task Force, IEEE 802.3 Plenary Session, Berlin, Germany, 10-12 March 2015cc

# Cu C2C SerDes & SMF Client TRX S/N (BtB, no FEC)

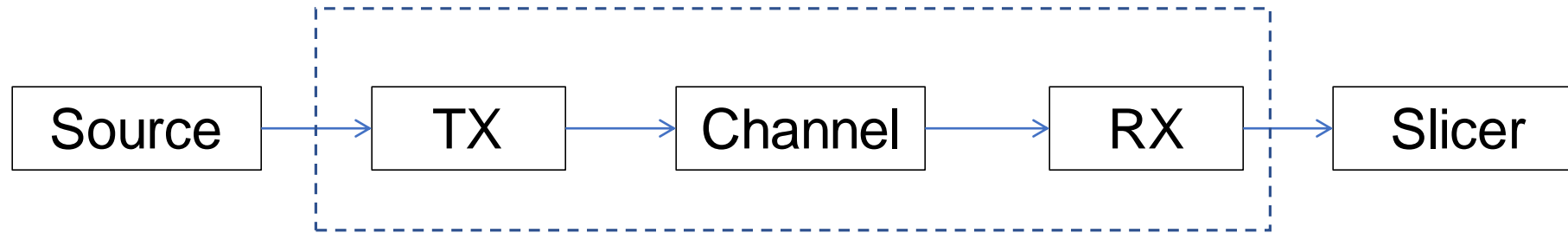


SMF client TRX:  
low S/N  
high B  
Shannon says: use NRZ

Cu C2C SerDes:  
high S/N  
low B  
Shannon says: use HOM

HOM  $\triangleq$  Higher Order Modulation

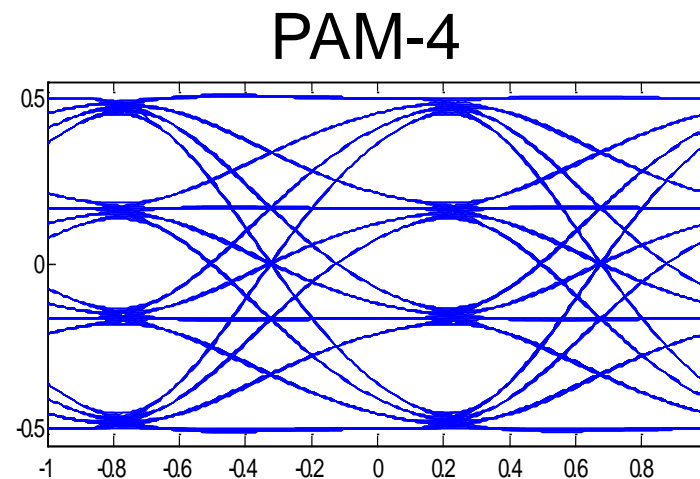
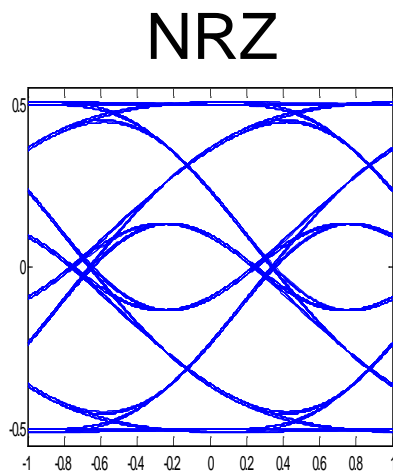
# Ideal SMF Client System Model



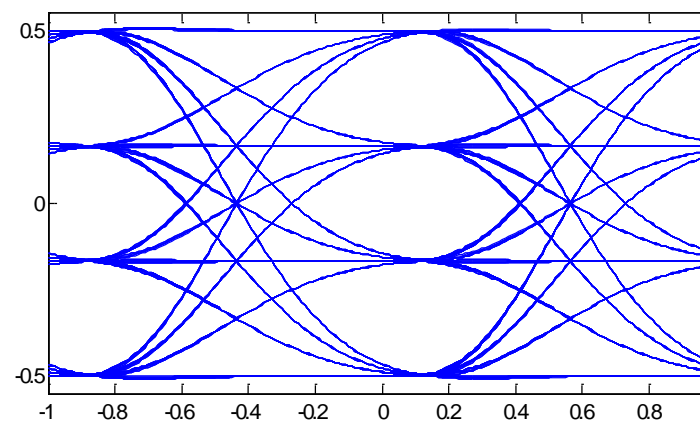
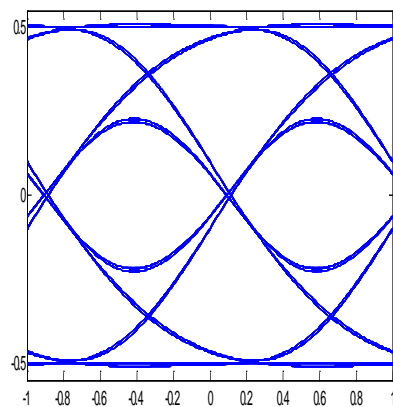
- SMF client channel ideal
- (TX \* Channel \* RX) modelled as 4th order BT filter
- $B = \alpha$  bit-rate
- Ex. bit rate = 56Gb/s
  - ex. 1:  $\alpha = 0.25 \rightarrow B = 14\text{GHz}$
  - ex. 2:  $\alpha = 0.30 \rightarrow B = 17\text{GHz}$

# Slicer Input Eyes of Ideal Noiseless SMF Client System

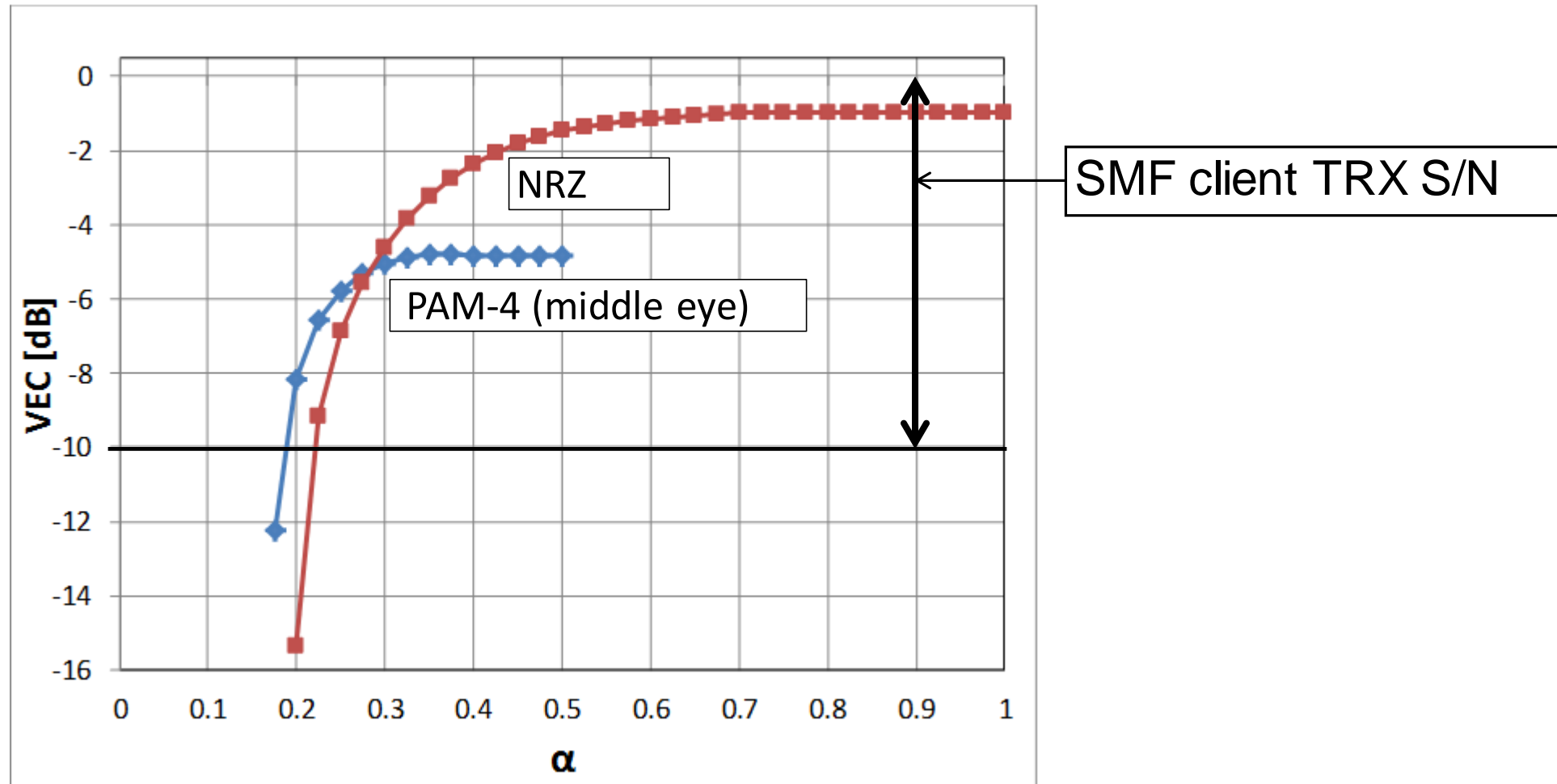
Ex. 1.  $\alpha = 0.25$  (14GHz)  
NRZ VEC  $\approx$  PAM4 VEC



Ex. 2.  $\alpha = 0.30$  (17GHz)  
NRZ VEC  $<$  PAM4 VEC



# Vertical Eye Closure at Slicer Input w/ Noise Normalization



# IEEE Modulation Choice for 50Gb/s and Faster Rates

- Optics is the tail on the IC industry dog
  - 50G PAM4 ASIC SerDes was first developed for the Cu channel
  - IC Vendors wanted to maximize their ADC and DSP investment
- IC dog wagged the optics tail
  - IEEE ignored Shannon
  - PAM4 standardized for 50G and 100G Ethernet optical lane rates
  - 200G (4x50G PAM4) FR4 will soon ship in the millions
- Optics & electronics today easily support 50G NRZ
  - Extra cost and power of 50G PAM4 ADC, DSP, SNR locked-in forever



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# Ethernet Optics History: 1 & 10GbE

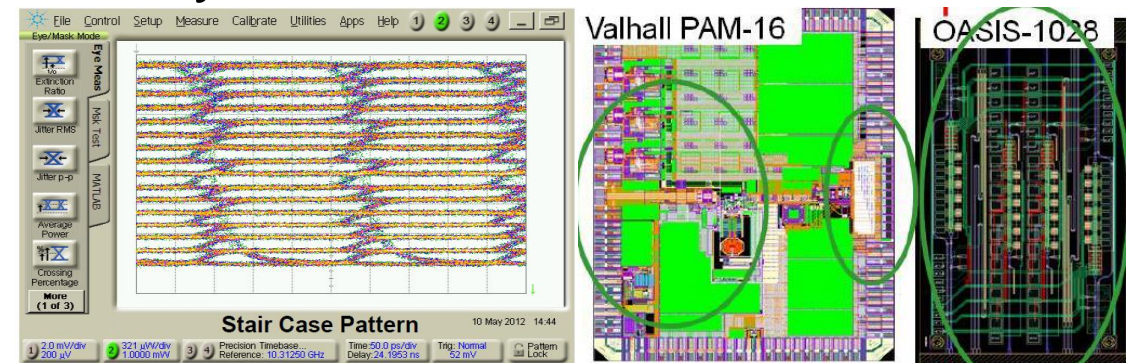
- 1GbE standard adopted in 1998
  - 1 $\lambda$  Serial NRZ (LX)
  - Shipped in the millions
- 10GbE standard adopted in 2002
  - 4 $\lambda$  WDM NRZ (LX4)
  - 1 $\lambda$  Serial NRZ (LR4)
  - 5-year delay in 10GbE adoption after 90's Tech bubble collapse
  - 10GBaud optics & electronics matured to easily support 10G NRZ
- 10G LR4 shipped in the millions
- 10G LX4 became a sad footnote in Ethernet optics history
- “Serial is always cheaper” myth is born

# Ethernet Optics History: 40GbE

- 40GbE standard adopted in 2010
  - “Serial is always cheaper” myth well established
  - Fierce debate in the IEEE between:
    - $4\lambda$  WDM NRZ (LR4) vs.
    - $1\lambda$  Serial NRZ (FR)
    - IEEE split the baby, adopted both
- 40G LR4 shipped in the millions
- 40G FR became a sad footnote in Ethernet optics history

# Ethernet Optics History: 100GbE

- 100GbE standard, targeted at the datacenter, adopted in 2015
  - “Serial is always cheaper” myth going strong
  - Fierce debate in the IEEE about duplex SMF spec between:
    - $4\lambda$  CWDM NRZ (FR4)
    - $1\lambda$  Serial PAM16/8 (FR)
    - IEEE could not reach agreement, and neither was adopted
- 100G CWDM4 spec developed immediately after in an MSA in 6 months
  - Shipped in the millions
- 100G PAM16/8 became a sad footnote in Ethernet optics history
- \$240M SNR math lesson for Cisco



# Ethernet Optics History: 400GbE

- 400GbE standard adopted in 2017
  - “Serial is always cheaper” myth unwavering
  - Fierce debate in the IEEE between:
    - $2\lambda$ \*50G WDM for 100G FR2 and  $8\lambda$ \*50G LWDM 400G LR8
    - $1\lambda$ \*100G Serial for 100G FR and 400G PSM DR4
    - IEEE split the baby, adopted 400G LR8 and DR4, but no 100G FR2
- 400G  $8\lambda$ \*50G LWDM LR8 shipped in low volume into early Telecom apps
- 400G  $4\lambda$ \*100G CWDM FR4 standardized soon afterwards

# Ethernet Optics History: 400GbE (2)

- Ethernet optics sad story 1: no Web2.0 deployment of 400GbE
  - Huge industry R&D investment into 1<sup>st</sup> Gen 400GbE FR4 with no ROI
  - 2<sup>nd</sup> Gen 400GbE FR4 will start shipping in volume in 2023 or later when Ethernet switches ship with 100G I/O
- Ethernet optics sad story 2: no low-cost, low-power 2 $\lambda$  100GbE optics matched to today's Ethernet switches with 50G I/O, forcing shipment of:
  - 4 $\lambda$  100G CWDM4 with 1:2 reverse gearbox (most Web2.0s), or
  - 1 $\lambda$  100G FR with with 2:1 forward gearbox (Amazon mainly)
  - Either way, significant cost and power added to 100G Ethernet optical links

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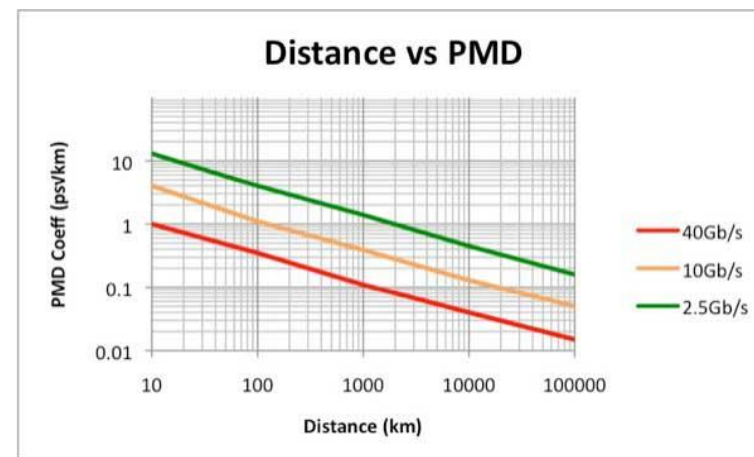
# G.652 SMF DWDM Transport C-band Spec Limits

- Loss
  - nom, max: 0.2, 0.28dB/km
  - **IF** link SNR was only determined by link loss
    - Coherent SNR  $\approx 2x$  IMDD SNR, in dB
    - Coherent reach  $\approx 2x$  IMDD reach, i.e. half the amplifier cost
- Bandwidth (B)
  - Spectral Efficiency is key metric because of fiber deployment cost
  - G.694.1 channel bandwidths: 25 to 100GHz
  - Coherent has 4 orthogonal channels: I, Q, TE, TM
  - Shannon says: If B limited, use S/N to increase modulation order

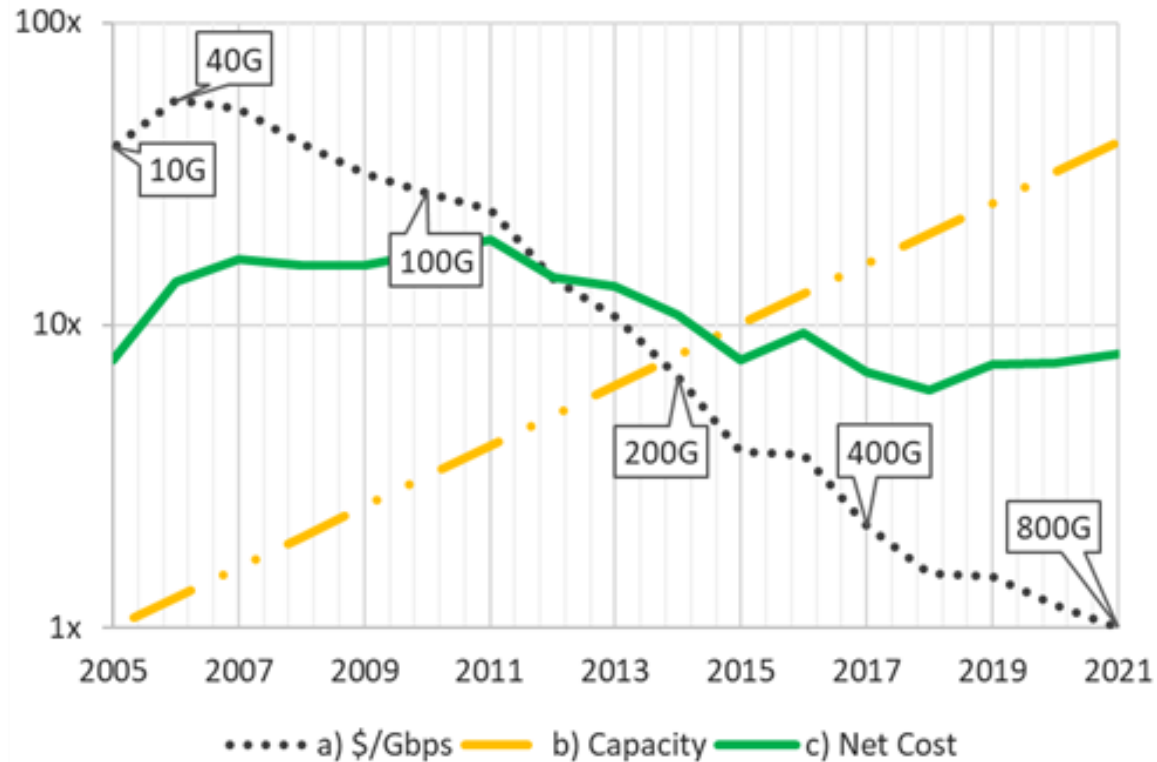


# G.652 SMF DWDM Transport C-band Spec Limits (2)

- Chromatic Dispersion (CD)
  - nom, max: 17, 20ps/nm-km
  - CD penalty variable with link reach
  - IMDD Fixed EQ: unique CDF length for each link
  - Coherent adaptive EQ: common for all links
- Polarization Mode Dispersion Q (PMDQ)
  - A&C nom:  $0.5\text{ps}/\sqrt{\text{km}}$
  - B&D nom:  $0.2\text{ps}/\sqrt{\text{km}}$
  - DGD is important over long reaches
  - Coherent adaptive EQ tracks polarization



# Transport Cost vs Time



10G - 40G: IMDD  
100G - 800G: Coherent

“A straight line will continue indefinitely as a straight line”

Optical Networks Forecast: 2018 – 2023, Jan 2019 Representative cost of optical transport capacity over time and transponder generations based on historical average sales price (ASP) of DWDM line card data from Ovum.

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# G.652 1km SMF CWDM4 O-band Spec Limits

- Loss
  - max: 0.47dB
  - Connectors and other passives determine link loss
  - Nom link loss budget: 4dB
  - SMF loss is not important
- Bandwidth (B)
  - 4 wavelength band: 10THz
  - 1 wavelength channel: 800GHz
  - Shannon says: If S/N limited, use B to increase Baud rate
  - SMF bandwidth is not important

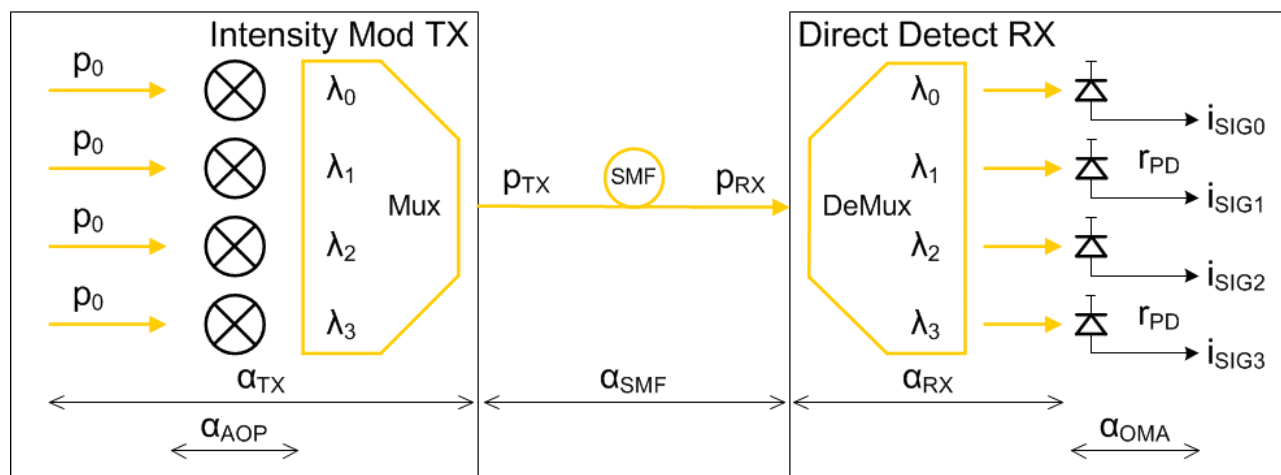
# G.652 1km SMF CWDM4 O-band Spec Limits (2)

- Chromatic Dispersion (CD)
  - min: -6ps/nm
  - max: 3ps/nm
  - SMF CD penalty is not important
- Polarization Mode Dispersion Q ( $PDM_Q$ )
  - A&C nom: 0.5ps
  - B&D nom: 0.2ps
  - SMF DGD penalty is not important

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# Direct Detection (DD) Signal Path



$$p_{\text{IN-TX}} = 4 p_0$$

$$p_{\text{TX}} = \alpha_{\text{AOP}} \alpha_{\text{TX}} p_{\text{IN-TX}}$$

$$i_{\text{SIG}} = \alpha_{\text{OMA}} r_{\text{PD}} p_{\text{PD}}$$

$$\sqrt{\text{snr}} = i_{\text{SIG}} / i_{\text{N}} = \alpha_{\text{OMA}} \alpha_{\text{RX}} \alpha_{\text{SMF}} \alpha_{\text{AOP}} \alpha_{\text{TX}} r_{\text{PD}} p_0 / (\alpha_{\text{N}} i_0 \sqrt{\text{BW}})$$

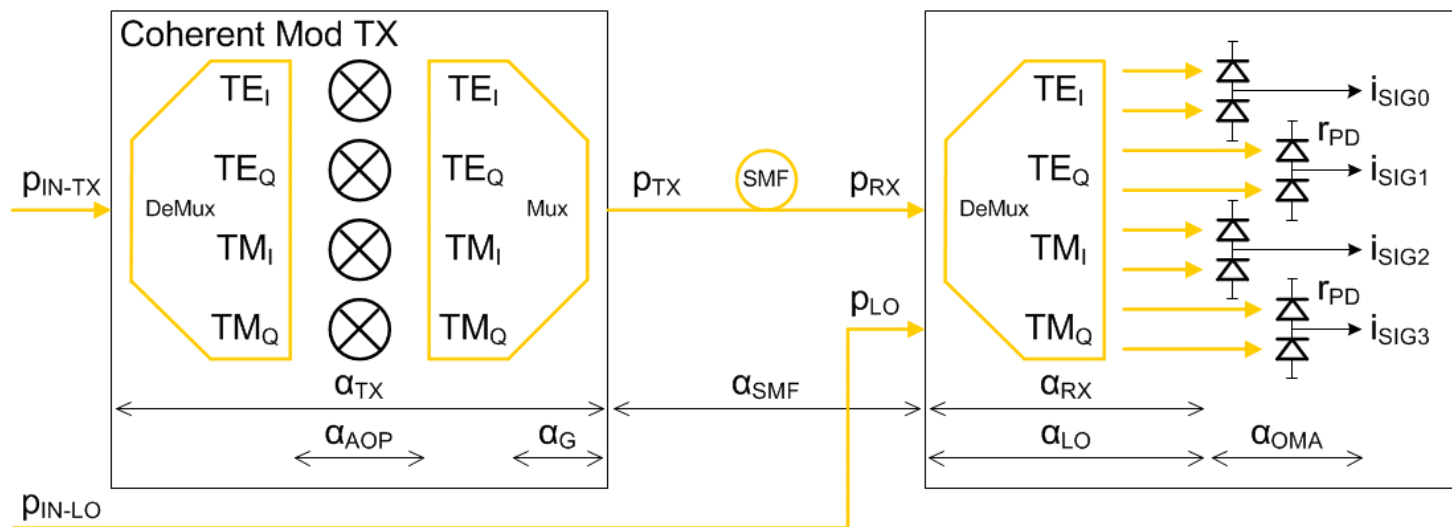
$$p_{\text{RX}} = \alpha_{\text{SMF}} p_{\text{TX}}$$

$$p_{\text{PD}} = \alpha_{\text{RX}} p_{\text{RX}} / 4$$

$$i_{\text{N}} = \alpha_{\text{N}} i_0 \sqrt{\text{BW}}$$

C. Cole, "Inside the Datacenter is not yet a Nail for the Coherent Hammer", WS05, Data Centers 1, Session 1, ECOC 2018, Rome, Italy, 23 Sep. 2018.

# Coherent (CH) Signal Path



$$p_{\text{IN-TX}} = 4 \alpha_{\text{LS}} \alpha_{\text{TEC}} p_0$$

$$p_{\text{TX}} = \alpha_{\text{G}} \alpha_{\text{OMA}} \alpha_{\text{TX}} p_{\text{IN-TX}}$$

$$p_{\text{LO}} = p_{\text{IN-LO}} = 4 (1 - \alpha_{\text{LS}}) \alpha_{\text{TEC}} p_0$$

$$i_{\text{SIG}} = \alpha_{\text{OMA}} r_{\text{PD}} 2 \sqrt{(p_{\text{PD-RX}} p_{\text{PD-LO}})}$$

$$\sqrt{\text{snr}} = i_{\text{SIG}} / i_{\text{N}} = \alpha_{\text{OMA}} \alpha_{\text{RX}} \sqrt{(\alpha_{\text{SMF}} \alpha_{\text{G}} \alpha_{\text{AOP}} \alpha_{\text{TX}}) \alpha_{\text{TEC}} r_{\text{PD}} p_0 / (\alpha_{\text{N}} i_0 \sqrt{\text{BW}})}$$

$$p_{\text{RX}} = \alpha_{\text{SMF}} \alpha_{\text{TX}}$$

$$p_{\text{PD-RX}} = \alpha_{\text{RX}} p_{\text{RX}} / 4$$

$$p_{\text{PD-LO}} = \alpha_{\text{LO}} p_{\text{LO}} / 4$$

$$i_{\text{N}} = \alpha_{\text{N}} i_0 \sqrt{\text{BW}}$$



$$\text{Optical } \Delta\text{SNR}_{\text{DD-CH}} = \text{SNR}_{\text{DD}} - \text{SNR}_{\text{CH}} \text{ dB}$$

$A \triangleq$  loss in optical -dB

$$A = -10\log_{10}(\alpha)$$

$$\Delta\text{SNR}_{\text{DD-CH}} = \text{SNR}_{\text{DD}} - \text{SNR}_{\text{CH}} = 10\log_{10}(\text{snr}_{\text{DD}} / \text{snr}_{\text{CH}})$$

$$\begin{aligned} \Delta\text{SNR}_{\text{DD-CH}}/2 = & - (A_{\text{AOP-DD}} + A_{\text{TX-DD}} + A_{\text{SMF}}) \\ & + (A_{\text{AOP-CH}} + A_{\text{TX-CH}} + A_{\text{G}} + A_{\text{SMF}})/2 + A_{\text{TEC}} \\ & - (A_{\text{OMA-DD}} + A_{\text{RX-DD}} - A_{\text{N-DD}}) \\ & + (A_{\text{OMA-CH}} + A_{\text{RX-CH}} - A_{\text{N-CH}}) \end{aligned}$$

$$A_{\text{TXT-DD}} = A_{\text{AOP-DD}} + A_{\text{TX-DD}} \qquad A_{\text{RXT-DD}} = A_{\text{OMA-DD}} + A_{\text{RX-DD}} - A_{\text{N-DD}}$$

$$A_{\text{TXT-CH}} = A_{\text{AOP-CH}} + A_{\text{TX-CH}} + A_{\text{G}} + 2A_{\text{TEC}} \qquad A_{\text{RXT-CH}} = A_{\text{OMA-CH}} + A_{\text{RX-CH}} - A_{\text{N-CH}}$$

$$\Delta\text{SNR}_{\text{DD-CH}} = (A_{\text{TXT-CH}} - 2A_{\text{TXT-DD}}) - A_{\text{SMF}} + 2(A_{\text{RXT-CH}} - A_{\text{RXT-DD}})$$

# Optical $\Delta\text{SNR}_{\text{DD-CH}}$ dB Link Loss Examples

- Equal laser input AOP (TEC ignored):

$$\Delta\text{SNR}_{\text{DD-CH}} = (A_{\text{TXT-CH}} - 2A_{\text{TXT-DD}}) - A_{\text{SMF}} + 2(A_{\text{RXT-CH}} - A_{\text{RXT-DD}})$$

- IMDD: 100G EML NRZ CWDM4

$$A_{\text{TXT-DD}} = 5\text{dB} \quad A_{\text{RXT-DD}} = 2\text{dB}$$

- Coherent: 100G SiPIC QPSK

$$A_{\text{TXT-CH}} = 17\text{dB} \quad A_{\text{RXT-CH}} = 4\text{dB}$$

- $A_{\text{SMF}} = \mathbf{4dB}$  ( 2km, typical intra datacenter)  $\Delta\text{SNR}_{\text{DD-CH}} = \mathbf{7dB}$
- $A_{\text{SMF}} = \mathbf{11dB}$  (20km, or 2km w/ 7dB switch loss)  $\Delta\text{SNR}_{\text{DD-CH}} = \mathbf{0}$
- $A_{\text{SMF}} = \mathbf{18dB}$  (40km, or 2km w/ 14dB switch loss)  $\Delta\text{SNR}_{\text{DD-CH}} = \mathbf{-7dB}$

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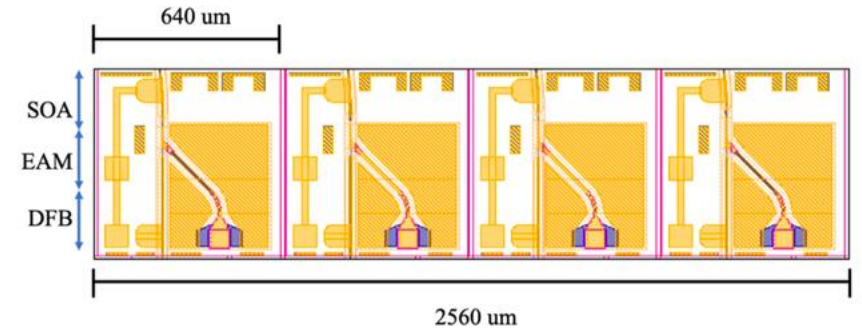
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# Intra Datacenter Optics Requirements

- What's important?
  - Cheap laser(s)
  - Cheap SNR (low loss components)
  - Cheap assembly and packaging
  - Cheap testing
- What does Coherent offer?
  - Expensive Laser
  - High loss components
  - Best case comparable packaging cost to IMDD
  - Complex testing

# TX Modulator Size Comparison

- IMDD InP EML length:
  - 400 - 500um (EA  $\approx$  120um)
- Coherent Si MZM length:
  - 2 - 4mm
- 4 channel Coherent to IMDD TX area ratio:
  - 10 - 20x



Teriphic project, 4x100G PAM4 EML TX

# Intra Datacenter Optics Today: Pluggable

- Characteristics
  - \$1 - \$2/Gb
  - ~30pJ/bit
  - IMDD DML or EML uncooled TX
  - 4λ CWDM NRZ or PAM4
  - Link budget: 4dB
- IMDD vs. Coherent SNR, equal laser DC Power (TEC included):  
100G EML NRZ CWDM4 IMDD vs 100G SiPIC QPSK Coherent  
 $\Delta\text{SNR}_{\text{DD-CH}} = 11.5\text{dB}$   
(same result for PAM4 IMDD vs QAM16 Coherent)

# Intra Datacenter Optics Tomorrow: Co-packaged

- Requirements
  - Co-packaged with Ethernet Switch ASIC
  - 256 - 512 data lanes
  - <\$1/Gb
  - <10pJ/bit
  - Link budget: 4dB
- IMDD vs. Coherent SNR, equal laser DC Power (TEC included):  
100G SiPIC NRZ CWDM4 IMDD vs 100G SiPIC QPSK Coherent  
 $\Delta\text{SNR}_{\text{DD-CH}} = 1.5\text{dB}$   
(same result for PAM4 IMDD vs QAM16 Coherent)

# Summary

- Coherent advantages in Transport are unimportant in Intra Datacenter
- Coherent indefinitely locks in the cost and power of ADCs and DSPs
  - This is what PAM4 did for >100G Ethernet optics
  - Good for IC vendors, bad for everyone else as optics improve
- “Serial is always cheaper” is a myth for leading data rates
  - 10GbE was the last time it was true
  - $1\lambda$  Coherent is higher cost and power than  $4\lambda$  IMDD
- Coherent does not reduce the cost and power of short reach optics
- There is no IMDD vs Coherent competition for Intra Datacenter links
  - Coherent is not even on the battleground



# IMDD vs Coherent

# Thank You

[www.ieee-sum.org](http://www.ieee-sum.org)



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- **Appendix 1**

# Direct Detection (DD) Signal Path Variables

$p_0$	$\triangleq$ Input POP (Peak Optical Power) reference
$p_{\text{IN-TX}}$	$\triangleq$ TX input POP = AOP (Average OP) if CW
$\alpha_{\text{AOP}}$	$\triangleq$ TX POP to AOP modulation loss vs. er (extinction ratio)
$\alpha_{\text{TX}}$	$\triangleq$ TX path intrinsic loss at modulator bias point
$p_{\text{TX}}$	$\triangleq$ TX total output AOP
$\alpha_{\text{SMF}}$	$\triangleq$ Link total power loss (connectors, SMF, other passives)
$p_{\text{RX}}$	$\triangleq$ RX total input AOP
$\alpha_{\text{RX}}$	$\triangleq$ RX path intrinsic loss
$p_{\text{PD}}$	$\triangleq$ RX PD input AOP
$r_{\text{PD}}$	$\triangleq$ RX PD responsivity
$\alpha_{\text{OMA}}$	$\triangleq$ PD AOP to average electrical signal power loss vs. er

# Direct Detection (DD) SNR

$V_{MD}$   $\triangleq$  TX modulator drive voltage

$i_{SIG}$   $\triangleq$  RX PD signal current

$$i_{SIG} = \alpha_{OMA} r_{PD} p_{PD} = \alpha_{OMA} \alpha_{RX} \alpha_{SMF} \alpha_{AOP} \alpha_{TX} r_{PD} p_0$$

$i_N$   $\triangleq$  RX input referred noise current; all sources

$i_0$   $\triangleq$  RX input noise current density reference

$\alpha_N$   $\triangleq$  RX input noise current loss vs.  $i_0$

BW  $\triangleq$  RX input noise bandwidth

$$i_N = \alpha_N i_0 \sqrt{BW}$$

$$snr = (i_{SIG} / i_N)^2$$

$$\sqrt{snr} = \alpha_{OMA} \alpha_{RX} \alpha_{SMF} \alpha_{AOP} \alpha_{TX} r_{PD} p_0 / (\alpha_N i_0 \sqrt{BW})$$

# Coherent (CH) Signal Path Variables

$p_0$	$\triangleq$ Input POP (Peak Optical Power) reference
$\alpha_{\text{TEC}}$	$\triangleq$ Input POP loss due to laser TEC current power
$\alpha_{\text{LS}}$	$\triangleq$ TX input POP loss due to $(1 - \alpha_{\text{LS}})$ LO (Local Oscillator) input split
$p_{\text{IN-TX}}$	$\triangleq$ TX input POP = AOP since CW
$\alpha_{\text{AOP}}$	$\triangleq$ TX POP to AOP modulation loss vs. $v_{\text{MD}}$ (mod. drive voltage)
$\alpha_{\text{TX}}$	$\triangleq$ TX path intrinsic loss at modulator bias point
$\alpha_{\text{G}}$	$\triangleq$ TX optical gain ( $\alpha_{\text{G}} = 1$ if no amplification)
$p_{\text{TX}}$	$\triangleq$ TX total output AOP
$\alpha_{\text{SMF}}$	$\triangleq$ Link total power loss (connectors, SMF, other passives)

## Coherent (CH) Signal Path Variables, cont.

$p_{RX}$   $\triangleq$  RX total input AOP

$p_{LO}$   $\triangleq$  RX LO input AOP

$\Phi(t)$   $\triangleq$  Phase angle between  $p_{RX}$  and  $p_{LO}$  electric fields

$\alpha_{RX}$   $\triangleq$  RX SIG path intrinsic loss

$\alpha_{LO}$   $\triangleq$  RX LO path intrinsic loss

$p_{PD}$   $\triangleq$  RX PD input AOP

$r_{PD}$   $\triangleq$  RX PD responsivity

$\alpha_{OMA}$   $\triangleq$  PD AOP to average electrical signal power loss vs.  $V_{MD}$

# Coherent Signal Addition

Optical signals, with same polarization state, add in the electric field domain

$$\begin{aligned}E_{\text{LO}} / \sqrt{Z} &\triangleq \sqrt{p_{\text{LO}}} \\E_{\text{RX}} / \sqrt{Z} &= \cos \Phi(t) \sqrt{p_{\text{RX}}} + j \sin \Phi(t) \sqrt{p_{\text{RX}}} \\E_{\text{PD}} / \sqrt{Z} &= \sqrt{p_{\text{LO}}} + \cos \Phi(t) \sqrt{p_{\text{RX}}} + j \sin \Phi(t) \sqrt{p_{\text{RX}}} \\P_{\text{PD}} &= (\sqrt{p_{\text{LO}}} + \cos \Phi(t) \sqrt{p_{\text{RX}}})^2 + (\sin \Phi(t) \sqrt{p_{\text{RX}}})^2 \\&= p_{\text{LO}} + 2 \sqrt{p_{\text{LO}}} \sqrt{p_{\text{RX}}} \cos \Phi(t) + p_{\text{RX}} \\p_{\text{RX}} &\ll 2 \sqrt{p_{\text{LO}}} \sqrt{p_{\text{RX}}} \cos \Phi(t) \\p_{\text{LO}} \text{ RIN} &\ll 2 \sqrt{p_{\text{LO}}} \sqrt{p_{\text{RX}}} \cos \Phi(t) \\p_{\text{PD}} &= 2 \sqrt{(p_{\text{LO}} p_{\text{RX}})} \cos \Phi(t)\end{aligned}$$

# Coherent (CH) SNR

$V_{MD}$   $\triangleq$  TX mod. drive voltage

$i_{SIG}$   $\triangleq$  RX balanced PD pair signal current

$i_{SIG} = \alpha_{OMA} r_{PD} 2 \sqrt{(p_{PD-RX} p_{PD-LO})} \cos \Phi(t)$

$\cos \Phi(t) \triangleq 1$        $\alpha_{LS} \triangleq 1/2$        $\alpha_{LO} \triangleq \alpha_{RX}$

$i_{SIG} = \alpha_{OMA} \alpha_{RX} \sqrt{(\alpha_{SMF} \alpha_G \alpha_{AOP} \alpha_{TX})} \alpha_{TEC} r_{PD} p_0$

$i_N$   $\triangleq$  RX input referred noise current; all sources

$i_0$   $\triangleq$  RX input noise current density reference

$\alpha_N$   $\triangleq$  RX input noise current loss vs.  $i_0$

$BW$   $\triangleq$  RX input noise bandwidth

$i_N = \alpha_N i_0 \sqrt{BW}$

$snr = (i_{SIG} / i_N)^2$

$\sqrt{snr} = \alpha_{OMA} \alpha_{RX} \sqrt{(\alpha_{SMF} \alpha_G \alpha_{AOP} \alpha_{TX})} \alpha_{TEC} r_{PD} p_0 / (\alpha_N i_0 \sqrt{BW})$



Ratio DD SNR to CH SNR:  $\sqrt{(\text{snr}_{\text{DD}} / \text{snr}_{\text{CH}})}$

$$\sqrt{\text{snr}_{\text{DD}}} = \alpha_{\text{OMA}} \alpha_{\text{RX}} \alpha_{\text{SMF}} \alpha_{\text{AOP}} \alpha_{\text{TX}} r_{\text{PD}} p_0 / (\alpha_{\text{N}} i_0 \sqrt{\text{BW}})$$

$$\sqrt{\text{snr}_{\text{CH}}} = \alpha_{\text{OMA}} \alpha_{\text{RX}} \sqrt{(\alpha_{\text{SMF}} \alpha_{\text{G}} \alpha_{\text{AOP}} \alpha_{\text{TX}})} \alpha_{\text{TEC}} r_{\text{PD}} p_0 / (\alpha_{\text{N}} i_0 \sqrt{\text{BW}})$$

$$r_{\text{PD-DD}} \triangleq r_{\text{PD-CH}}$$

$$\text{BW}_{\text{DD}} \triangleq \text{BW}_{\text{CH}}$$

$$\begin{aligned} \sqrt{(\text{snr}_{\text{DD}} / \text{snr}_{\text{CH}})} &= \alpha_{\text{OMA-DD}} \alpha_{\text{RX-DD}} \alpha_{\text{SMF}} \alpha_{\text{AOP-DD}} \alpha_{\text{TX-DD}} \alpha_{\text{N-CH}} \\ &\quad / \alpha_{\text{OMA-CH}} \alpha_{\text{RX-CH}} \sqrt{(\alpha_{\text{SMF}} \alpha_{\text{G}} \alpha_{\text{AOP-CH}} \alpha_{\text{TX-CH}})} \alpha_{\text{TEC}} \alpha_{\text{N-DD}} \end{aligned}$$

$$\text{Optical } \Delta\text{SNR}_{\text{DD-CH}} = \text{SNR}_{\text{DD}} - \text{SNR}_{\text{CH}} \text{ dB}$$

$A \triangleq$  loss in optical -dB

$$A = -10\log_{10}(\alpha)$$

$$\Delta\text{SNR}_{\text{DD-CH}} = \text{SNR}_{\text{DD}} - \text{SNR}_{\text{CH}} = 10\log_{10}(\text{snr}_{\text{DD}} / \text{snr}_{\text{CH}})$$

$$\begin{aligned} \Delta\text{SNR}_{\text{DD-CH}}/2 = & - (A_{\text{AOP-DD}} + A_{\text{TX-DD}} + A_{\text{SMF}}) \\ & + (A_{\text{AOP-CH}} + A_{\text{TX-CH}} + A_{\text{G}} + A_{\text{SMF}})/2 + A_{\text{TEC}} \\ & - (A_{\text{OMA-DD}} + A_{\text{RX-DD}} - A_{\text{N-DD}}) \\ & + (A_{\text{OMA-CH}} + A_{\text{RX-CH}} - A_{\text{N-CH}}) \end{aligned}$$

$$A_{\text{TX-T-DD}} = A_{\text{AOP-DD}} + A_{\text{TX-DD}}$$

$$A_{\text{RX-T-DD}} = A_{\text{OMA-DD}} + A_{\text{RX-DD}} - A_{\text{N-DD}}$$

$$A_{\text{TX-T-CH}} = A_{\text{AOP-CH}} + A_{\text{TX-CH}} + A_{\text{G}} + 2A_{\text{TEC}}$$

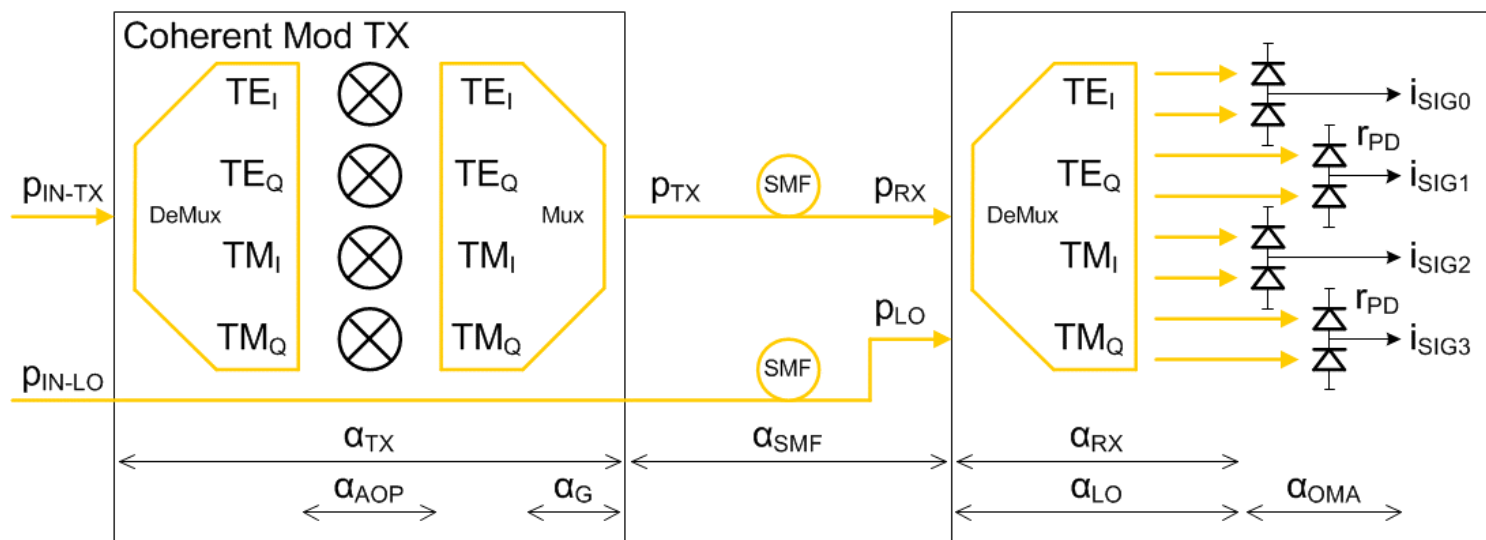
$$A_{\text{RX-T-CH}} = A_{\text{OMA-CH}} + A_{\text{RX-CH}} - A_{\text{N-CH}}$$

$$\Delta\text{SNR}_{\text{DD-CH}} = (A_{\text{TX-T-CH}} - 2A_{\text{TX-T-DD}}) - A_{\text{SMF}} + 2(A_{\text{RX-T-CH}} - A_{\text{RX-T-DD}})$$

# Outline

- NRZ vs HOM
- Serial vs WDM
- Coherent in Telecom
- Coherent in Datacom
- IMDD vs Coherent SNR
- Intra Datacenter Optics
- **Appendix 2**

# Coherent (CH) w/ same TX Signal & LO Path



$$p_{\text{IN-TX}} = 4 \alpha_{\text{LS}} \alpha_{\text{TEC}} p_0$$

$$p_{\text{TX}} = \alpha_{\text{G}} \alpha_{\text{AOP}} \alpha_{\text{TX}} p_{\text{IN-TX}}$$

$$p_{\text{IN-LO}} = 4 (1 - \alpha_{\text{LS}}) \alpha_{\text{TEC}} p_0$$

$$i_{\text{SIG}} = \alpha_{\text{OMA}} r_{\text{PD}} 2 \sqrt{(p_{\text{PD-RX}} p_{\text{PD-LO}})}$$

$$p_{\text{RX}} = \alpha_{\text{SMF}} \alpha_{\text{TX}}$$

$$p_{\text{PD-RX}} = \alpha_{\text{RX}} p_{\text{RX}} / 4$$

$$p_{\text{PD-LO}} = \alpha_{\text{LO}} \alpha_{\text{SMF}} \alpha_{\text{G}} \alpha_{\text{AOP}} \alpha_{\text{TX}} p_{\text{IN-LO}} / 4$$

$$i_{\text{N}} = \alpha_{\text{N}} i_0 \sqrt{\text{BW}}$$

# Coherent (CH) RX Signal w/ same TX Signal & LO Path

$i_{\text{SIG}} \triangleq$  RX balanced PD pair signal current

$$i_{\text{SIG}} = \alpha_{\text{OMA}} r_{\text{PD}} 2 \sqrt{(p_{\text{PD-RX}} p_{\text{PD-LO}})}$$

$$\alpha_{\text{LS}} \triangleq 1/2 \quad \alpha_{\text{LO}} \triangleq \alpha_{\text{RX}}$$

$$i_{\text{SIG}} = \alpha_{\text{OMA}} \alpha_{\text{RX}} \alpha_{\text{SMF}} \alpha_{\text{G}} \alpha_{\text{AOP}} \alpha_{\text{TX}} \alpha_{\text{TEC}} r_{\text{PD}} p_0$$

Equal DD and CH total input AOP condition:

$$p_{\text{IN-DD-TX}} \triangleq p_{\text{IN-CH-TX}} + p_{\text{IN-CH-LO}}$$

$$i_{\text{DD-SIG}} = i_{\text{CH-SIG}}$$

When the LO is remote, i.e. it's a RO, there is no Coherent signal gain!

Same TX Signal and LO Path analysis approach proposed by Mike Frankel, Ciena, 18 Jan 2018.

# Outline

- NRZ vs HOM
- Serial vs WDM
- Coherent in Telecom
- Coherent in Datacom
- IMDD vs Coherent SNR
- Intra Datacenter Optics
- **Appendix 3**

# $\Delta\text{SNR}_{\text{DD-CH}} = \text{SNR}_{\text{DD}} - \text{SNR}_{\text{CH}}$ Examples

$$\Delta\text{SNR}_{\text{DD-CH}}/2 =$$

- $A_{\text{TX-DD}} + A_{\text{TX-CH}}/2$  // TX intrinsic
- $A_{\text{AOP-DD}} + A_{\text{AOP-CH}}/2$  // TX POP to AOP
- $A_{\text{G}}/2 + A_{\text{TEC}}$  // TX scenarios
- $A_{\text{SMF}}/2$  // Link
- $A_{\text{RX-DD}} + A_{\text{RX-CH}}$  // RX intrinsic
- $A_{\text{OMA-DD}} + A_{\text{OMA-CH}}$  // RX AOP to average electrical
- $(-A_{\text{N-DD}}) + (-A_{\text{N-CH}})$  // RX noise

# TX Signal Path Intrinsic Loss Values

- $A_{TX} \triangleq$  TX path intrinsic loss, -dB

Ex. #	Implementation	DD loss value -dB	CH loss value -dB
		$A_{TX-DD}$	$A_{TX-CH}$
1	Ideal TX & RX, no loss	0	0
2	DD CWDM4 TFF DML TX, RX CH SiP	4	14
3	DD CWDM4 TFF EML TX, RX CH SiP (ECOC'18 WS Example)	5	14
4	DD PSM4 SiP TX & RX CH SiP	6	14
5	DD CWDM4 SiP TX & RX, CH SiP	8	14



# TX Modulation Loss

- $\alpha_{\text{AOP}}, A_{\text{AOP}} \triangleq$  TX input POP to AOP modulation loss; linear, -dB
- $\alpha_{\text{AOP-NRZ}} [\text{er}] = (\text{er} + 1) / (2 \text{er})$  // Mod. TX POP to AOP loss
- $\alpha_{\text{AOP-NRZ}} [\text{er}] = 1$  // DML TX, no loss
- $\alpha_{\text{AOP-PAM4}} [\text{er}] = (\text{er} + 1) / (2 \text{er})$  // Mod. TX POP to AOP loss
- $\alpha_{\text{AOP-PAM4}} [\text{er}] = 1$  // DML TX, no loss
- $\alpha_{\text{AOP-QPSK}} [V_{\text{MD}} = 2V_{\pi}] = 1$
- $\alpha_{\text{AOP-QPSK}} [V_{\text{MD}} = V_{\pi}] = 1/2$
- $\alpha_{\text{AOP-QAM16}} [V_{\text{MD}} = 2V_{\pi}] = 5/9$
- $\alpha_{\text{AOP-QAM16}} [V_{\text{MD}} = V_{\pi}] = 5/18$
- Equal DD & CH TX modulation drive
  - $V_{\text{MD-DD(max)}} \triangleq \frac{1}{2} V_{\text{MD-CH(max)}}$
  - $V_{\text{MD-CH}} = V_{\pi}$

# TX Modulation Loss Values

- $A_{\text{AOP}} \triangleq$  TX input POP to AOP modulation loss, -dB

mod. loss variable	ER dB	DD mod. loss value -dB		DD DM loss value -dB	
		NRZ	PAM4	NRZ	PAM4
$A_{\text{AOP-DD}}$	$\infty$	3.0	3.0	0.0	0.0
	7	2.2	2.2	0.0	0.0
	4.8	1.8	1.8	0.0	0.0

mod. loss variable	$V_{\text{MD}}$	CH loss value -dB		CH loss value -dB / 2	
		QPSK	QAM16	QPSK	QAM16
$A_{\text{AOP-CH}}$	$2V_{\text{TT}}$	0.0	2.6	0.0	1.3
	$V_{\text{TT}}$	3.0	5.6	1.5	2.8

# TX Scenarios

- $\alpha_{\text{TEC}}, A_{\text{TEC}}$   $\triangleq$  TX<sub>CH</sub> input POP loss, laser TEC current; linear, -dB
- $\alpha_{\text{G}}, A_{\text{G}}$   $\triangleq$  TX<sub>CH</sub> optical gain expressed as loss
- Scenario 1: equal laser DC power (40% efficient CH TEC)
  - $i_{\text{Laser-bias-DD}}$   $\triangleq$   $i_{\text{Laser-bias-CH}} + i_{\text{Laser-TEC-CH}}$
  - $\alpha_{\text{TEC}}$   $\triangleq$  0.4
  - $\alpha_{\text{G}}$   $\triangleq$  1
- Scenario 2: equal TX & LO total input POP (no CH TEC)
  - $p_{\text{IN-TX-DD}}$   $\triangleq$   $p_{\text{IN-TX-CH}} + p_{\text{IN-LO-CH}}$
  - $\alpha_{\text{TEC}}$   $\triangleq$  1
  - $\alpha_{\text{G}}$   $\triangleq$  1

# TX Scenarios, cont.

- Scenario 3: equal TX total output AOP (no DC power limit)

$$p_{\text{TX-DD}} \triangleq p_{\text{TX-CH}}$$

$$A_{\text{TX-DD}} + A_{\text{AOP-DD}} = A_G + A_{\text{TX-CH}} + A_{\text{AOP-CH}} + A_{\text{LS}} + A_{\text{TEC}}$$

$$\alpha_{\text{TEC}} \triangleq 1$$

$$A_{\text{TEC}} = 0$$

$$\alpha_{\text{LS}} \triangleq 1/2$$

$$A_{\text{LS}} = 3$$

$$- A_G / 2 = ((A_{\text{TX-CH}} + A_{\text{AOP-CH}} + 3) - (A_{\text{TX-DD}} + A_{\text{AOP-DD}})) / 2$$

# TX Scenarios Loss Values

- $A_G \triangleq \text{TX}_{\text{CH}}$  optical gain expressed as loss
- $A_{\text{TEC}} \triangleq \text{TX}_{\text{CH}}$  input POP loss due to laser TEC current, -dB

	$\Delta\text{SNR}_{\text{DD-CH}} / 2$ TX Scenario	CH loss variable	CH loss value -dB	CH loss variable	CH loss value -dB
1	Equal laser DC power	$A_G / 2$	0	$A_{\text{TEC}}$	4
2	Equal total input AOP	$A_G / 2$	0	$A_{\text{TEC}}$	0
3	Equal TX total output AOP	$A_G / 2$	<i>formula on p.52</i>	$A_{\text{TEC}}$	0

# TX Scenarios: Coherent Unequal SIG/LO Split Loss

- $\alpha_{ALS}, A_{ALS}$   $\triangleq$  Unequal SIG/LO split  $\alpha_{LS} \neq 1/2$  loss; linear, -dB  
 $\alpha_{ALS} = 2 \sqrt{\alpha_{LS} (1 - \alpha_{LS})}$   
 $\alpha_{LS} \triangleq 1/2$   
 $A_{ALS} = 0$   
 $\alpha_{LS} \triangleq 2/3$   
 $A_{ALS} = 0.3$
- $A'_{OMA-CH} = A_{OMA-CH} + A_{ALS}$

mod. loss variable	$V_{MD}$	CH loss value -dB			
		$\alpha_{LS} = 1/2$		$\alpha_{LS} = 2/3$	
		QPSK	QAM16	QPSK	QAM16
$A'_{OMA-CH}$	$2V_{\pi}$	0.0	0.0	0.3	0.3
	$V_{\pi}$	0.0	0.0	0.3	0.3

# Link Loss Values

- $A_{\text{SMF}} \triangleq$  Link total power loss (connectors, SMF, other passives), -dB
- Standard datacenter link loss budget  
 $A_{\text{SMF}} \triangleq 4$

DD loss value -dB	CH loss value -dB
$A_{\text{SMF}}$	$A_{\text{SMF}} / 2$
4.0	2.0

# RX Signal Path Intrinsic Loss Values

- $A_{RX} \triangleq$  RX path intrinsic loss, -dB
- $A_{LO} \triangleq$  RX LO path intrinsic loss, -dB:  $A_{LO-CH} \triangleq A_{RX-CH}$

Ex. #	Implementation	DD loss value -dB	CH loss value -dB
		$A_{RX-DD}$	$A_{RX-CH}$
1	Ideal TX & RX, no loss	0	0
2	DD CWDM4 TFF DML TX, RX CH SiP	2	4
3	DD CWDM4 TFF EML TX, RX CH SiP (ECOC'18 WS Example)	2	4
4	DD PSM4 SiP TX & RX CH SiP	2	4
5	DD CWDM4 SiP TX & RX, CH SiP	4	4



# RX Modulation Loss

- $\alpha_{\text{OMA}}, A_{\text{OMA}} \triangleq$  RX PD AOP to average electrical signal power loss; linear, -dB
- $\alpha_{\text{OMA-NRZ}} [\text{er}] = (\text{er} - 1) / (\text{er} + 1) \quad // \frac{1}{2} * \text{AOP to OMA loss}$
- $\alpha_{\text{OMA-PAM4}} [\text{er}] = \sqrt{(5/9)} (\text{er} - 1) / (\text{er} + 1) \quad // \frac{1}{2} * \text{AOP to OMA loss}$
- $\alpha_{\text{OMA-QPSK}} [V_{\text{MD}} = 2V_{\pi}] = 1$
- $\alpha_{\text{OMA-QPSK}} [V_{\text{MD}} = V_{\pi}] = 1$
- $\alpha_{\text{OMA-QAM16}} [V_{\text{MD}} = 2V_{\pi}] = 1$
- $\alpha_{\text{OMA-QAM16}} [V_{\text{MD}} = V_{\pi}] = 1$
- Equal DD & CH TX modulation drive
  - $V_{\text{MD-DD(max)}} \triangleq \frac{1}{2} V_{\text{MD-CH(max)}}$
  - $V_{\text{MD-CH}} = V_{\pi}$

# RX Modulation Loss Values

- $A_{\text{OMA}} \triangleq$  RX PD AOP to average electrical signal power loss, -dB

Mod. loss variable	ER dB	DD Mod. loss value -dB		DD DM loss value -dB	
		NRZ	PAM4	NRZ	PAM4
$A_{\text{OMA-DD}}$	$\infty$	0.0	1.3	<i>0.0</i>	<i>1.3</i>
	7	1.8	3.0	<i>1.8</i>	<i>3.0</i>
	4.8	<i>3.0</i>	<i>4.3</i>	3.0	4.3

Mod. loss variable	$V_{\text{MD}}$	CH loss value -dB	
		QPSK	QAM16
$A_{\text{OMA-CH}}$	$2V_{\pi}$	<i>0.0</i>	<i>0.0</i>
	$V_{\pi}$	0.0	0.0

# RX Input Referred Noise Current Loss Values

- $A_N$   $\triangleq$  RX input noise current density loss vs. reference, -dB
- $\alpha_N i_0$   $\triangleq$  RX input noise current density
- RX input noise current density values
  - $\alpha_{N-DD} i_0 = 12\text{pA} / \sqrt{\text{Hz}}$
  - $\alpha_{N-DD} \triangleq 1$
  - $i_0 = 12\text{pA} / \sqrt{\text{Hz}}$
  - $\alpha_{N-CH} i_0 = 20\text{pA} / \sqrt{\text{Hz}}$
  - $\alpha_{N-CH} = 5/3$

DD loss value -dB	CH loss value -dB
$A_{N-DD}$	$A_{N-CH}$
0.0	-2.2

# Ex.1: $\Delta\text{SNR}_{\text{DD-CH}}/2$ Ideal TX & RX no loss

Ex. 1 $\Delta\text{SNR}_{\text{DD-CH}}/2$ dB		DD loss var.	DD Ideal TX ER = $\infty$ loss value -dB		CH loss var.	CH Ideal TX $v_{\text{MD}} = V_{\text{TT}}$ loss value -dB	
Loss Type		$A_{\text{DD}}$	NRZ	PAM4	$A_{\text{CH}}$	QPSK	QAM16
TX		$A_{\text{AOP}}$	3.0	3.0	$A_{\text{AOP}}/2$	1.5	2.8
		$A_{\text{TX}}$	0		$A_{\text{TX}}/2$	0	
1	Equal laser DC power	n/a	0.0		$A_{\text{G}}/2$ $+ A_{\text{TEC}}$	4.0	
2	Equal total input AOP		0.0			0.0	
3	Equal TX output AOP		0.0			-1.5	-2.8
Link		$A_{\text{SMF}}$	4		$A_{\text{SMF}}/2$	2	
RX		$A_{\text{RX}}$	0		$A_{\text{RX}}$	0	
		$A_{\text{OMA}}$	0.0	1.3	$A_{\text{OMA}}$	0.0	0.0
		$-A_{\text{N}}$	0.0		$-A_{\text{N}}$	2.2	
1. Equal laser DC power		2. Equal total input AOP			3. Equal TX output AOP		
NRZ - QPSK	PAM4 - QAM16	NRZ - QPSK	PAM4 - QAM16	NRZ - QPSK	PAM4 - QAM16		
<b>2.7</b>	<b>2.7</b>	<b>-1.3</b>	<b>-1.3</b>	<b>-2.8</b>	<b>-4.1</b>		

# Ex.2: $\Delta\text{SNR}_{\text{DD-CH}}/2$ DD CWDM TFF, DML TX

Ex. 2 $\Delta\text{SNR}_{\text{DD-CH}}/2$ dB		DD loss var.	DD CWDM4 TFF, DML TX ER = 4.8 loss value -dB		CH loss var.	CH SiP TX $v_{\text{MD}} = V_{\text{TT}}$ loss value -dB	
Loss Type		$A_{\text{DD}}$	NRZ	PAM4	$A_{\text{CH}}$	QPSK	QAM16
TX		$A_{\text{AOP}}$	0.0	0.0	$A_{\text{AOP}}/2$	1.5	2.8
		$A_{\text{TX}}$	4		$A_{\text{TX}}/2$	7	
1	Equal laser DC power	n/a	0.0		$A_{\text{G}}/2$ + $A_{\text{TEC}}$	4.0	
2	Equal total input AOP		0.0			0.0	
3	Equal TX output AOP		0.0			-8.0	-9.3
Link		$A_{\text{SMF}}$	4		$A_{\text{SMF}}/2$	2	
RX		$A_{\text{RX}}$	2		$A_{\text{RX}}$	4	
		$A_{\text{OMA}}$	3.0	4.3	$A_{\text{OMA}}$	0.0	0.0
		$-A_{\text{N}}$	0.0		$-A_{\text{N}}$	2.2	
1. Equal laser DC power		2. Equal total input AOP			3. Equal TX output AOP		
NRZ - QPSK	PAM4 - QAM16	NRZ - QPSK	PAM4 - QAM16	NRZ - QPSK	PAM4 - QAM16		
<b>7.7</b>	<b>7.7</b>	<b>3.7</b>	<b>3.7</b>	<b>-4.3</b>	<b>-5.5</b>		

# Ex.3: $\Delta\text{SNR}_{\text{DD-CH}}/2$ DD CWDM4 TFF, EML TX

Ex. 3 (ECOC'18 WS Ex.) $\Delta\text{SNR}_{\text{DD-CH}}/2$ dB		DD loss var.	DD CWDM4 TFF, EML TX ER = 7 loss value -dB		CH loss var.	CH SiP TX $V_{\text{MD}} = V_{\text{TT}}$ loss value -dB	
Loss Type		$A_{\text{DD}}$	NRZ	PAM4	$A_{\text{CH}}$	QPSK	QAM16
TX		$A_{\text{AOP}}$	2.2	2.2	$A_{\text{AOP}}/2$	1.5	2.8
		$A_{\text{TX}}$	5		$A_{\text{TX}}/2$	7	
1	Equal laser DC power	n/a	0.0		$A_{\text{G}}/2$ + $A_{\text{TEC}}$	4.0	
2	Equal total input AOP		0.0			0.0	
3	Equal TX output AOP		0.0			-6.4	-7.7
Link		$A_{\text{SMF}}$	4		$A_{\text{SMF}}/2$	2	
RX		$A_{\text{RX}}$	2		$A_{\text{RX}}$	4	
		$A_{\text{OMA}}$	1.8	3.0	$A_{\text{OMA}}$	0.0	0.0
		$-A_{\text{N}}$	0.0		$-A_{\text{N}}$	2.2	
1. Equal laser DC power		2. Equal total input AOP			3. Equal TX output AOP		
NRZ - QPSK	PAM4 - QAM16	NRZ - QPSK	PAM4 - QAM16	NRZ - QPSK	PAM4 - QAM16		
<b>5.7</b>	<b>5.7</b>	<b>1.7</b>	<b>1.7</b>	<b>-4.6</b>	<b>-5.9</b>		

# Ex.4: $\Delta\text{SNR}_{\text{DD-CH}}/2$ DD PSM4 SiP

Ex. 4 $\Delta\text{SNR}_{\text{DD-CH}}/2$ dB		DD loss var.	DD PSM4 SiP TX ER = 7 loss value -dB		CH loss var.	CH SiP TX $v_{\text{MD}} = V_{\text{TT}}$ loss value -dB	
Loss Type		$A_{\text{DD}}$	NRZ	PAM4	$A_{\text{CH}}$	QPSK	QAM16
TX		$A_{\text{AOP}}$	2.2	2.2	$A_{\text{AOP}}/2$	1.5	2.8
		$A_{\text{TX}}$	6		$A_{\text{TX}}/2$	7	
1	Equal laser DC power	n/a	0.0		$A_{\text{G}}/2$ + $A_{\text{TEC}}$	4.0	
2	Equal total input AOP		0.0			0.0	
3	Equal TX output AOP		0.0			-5.9	-7.2
Link		$A_{\text{SMF}}$	4		$A_{\text{SMF}}/2$	2	
RX		$A_{\text{RX}}$	2		$A_{\text{RX}}$	4	
		$A_{\text{OMA}}$	1.8	3.0	$A_{\text{OMA}}$	0.0	0.0
		$-A_{\text{N}}$	0.0		$-A_{\text{N}}$	2.2	
1. Equal laser DC power		2. Equal total input AOP			3. Equal TX output AOP		
NRZ - QPSK	PAM4 - QAM16	NRZ - QPSK	PAM4 - QAM16	NRZ - QPSK	PAM4 - QAM16		
<b>4.7</b>	<b>4.7</b>	<b>0.7</b>	<b>0.7</b>	<b>-5.1</b>	<b>-6.4</b>		

# Ex.5: $\Delta\text{SNR}_{\text{DD-CH}}/2$ DD CWDM4 SiP

Ex. 5 $\Delta\text{SNR}_{\text{DD-CH}}/2$ dB		DD loss var.	DD CWDM4 SiP TX ER = 7 loss value -dB		CH loss var.	CH SiP TX $v_{\text{MD}} = v_{\text{TT}}$ loss value -dB	
Loss Type		$A_{\text{DD}}$	NRZ	PAM4	$A_{\text{CH}}$	QPSK	QAM16
TX		$A_{\text{AOP}}$	2.2	2.2	$A_{\text{AOP}}/2$	1.5	2.8
		$A_{\text{TX}}$	8		$A_{\text{TX}}/2$	7	
1	Equal laser DC power	n/a	0.0		$A_{\text{G}}/2$ + $A_{\text{TEC}}$	4.0	
2	Equal total input AOP		0.0			0.0	
3	Equal TX output AOP		0.0			-4.9	-6.2
Link		$A_{\text{SMF}}$	4		$A_{\text{SMF}}/2$	2	
RX		$A_{\text{RX}}$	4		$A_{\text{RX}}$	4	
		$A_{\text{OMA}}$	1.8	3.0	$A_{\text{OMA}}$	0.0	0.0
		$-A_{\text{N}}$	0.0		$-A_{\text{N}}$	2.2	
1. Equal laser DC power		2. Equal total input AOP			3. Equal TX output AOP		
NRZ - QPSK	PAM4 - QAM16	NRZ - QPSK	PAM4 - QAM16	NRZ - QPSK	PAM4 - QAM16		
<b>0.7</b>	<b>0.7</b>	<b>-3.3</b>	<b>-3.3</b>	<b>-8.1</b>	<b>-9.4</b>		



# $\Delta\text{SNR}_{\text{DD-CH}}$ dB Examples, 4dB SMF Link Loss

$\Delta\text{SNR}_{\text{DD-CH}}$ dB		Scenario		1. Equal laser DC power		2. Equal total input AOP		3. Equal TX output AOP	
Ex. #	TX & RX Implementation	NRZ - QPSK	PAM4 - QAM16	NRZ - QPSK	PAM4 - QAM16	NRZ - QPSK	PAM4 - QAM16	NRZ - QPSK	PAM4 - QAM16
1	Ideal TX & RX no loss DD ER = $\infty$ , CH $v_{\text{MD}} = V_{\text{T}}$	5.4		-2.6		-5.6		-8.1	
2	DD CWDM4 TFF DML TX ER = 4.8, SiP CH $v_{\text{MD}} = V_{\text{T}}$	15.4		7.4		-8.6		-11.1	
3	DD CWDM4 TFF EML TX ER = 7, SiP CH $v_{\text{MD}} = V_{\text{T}}$	11.5		3.5		-9.3		-11.8	
4	DD PSM4 SiP TX ER = 7, SiP CH $v_{\text{MD}} = V_{\text{T}}$	9.5		1.5		-10.3		-12.8	
5	DD CWDM4 SiP TX ER = 7, SiP CH $v_{\text{MD}} = V_{\text{T}}$	1.5		-6.5		-16.3		-18.8	

# Coherent vs. IMDD SNR Examples Conclusion

Application	Direct Detection NRZ / PAM4 SNR		SNR Relation	Coherent QPSK / QAM16 SNR	
	TX	RX		TX	RX
Laser DC Power Constrained	EML, DML single $\lambda$ or TFF, PLC WDM	PIN single $\lambda$ or TFF, PLC WDM	$\gg$	SiP	SiP
	single $\lambda$ SiP (PSM)	single $\lambda$ SiP (PSM)	$\gg$	SiP	SiP
4dB Link Loss	WDM SiP	WDM SiP	$\approx$	SiP	SiP
TX Out Power Constrained	Any	PIN	$\ll$	SiP	SiP

For most intra datacenter links, IMDD has better SNR than Coherent, contrary to conventional wisdom.

# IMDD vs Coherent Appendices

## Thank You

[www.ieee-sum.org](http://www.ieee-sum.org)

